

FIG. 1

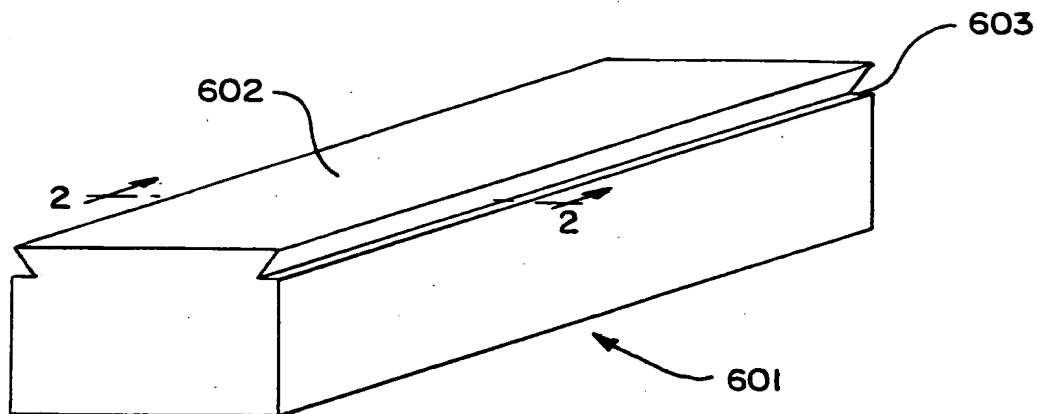


FIG. 2A

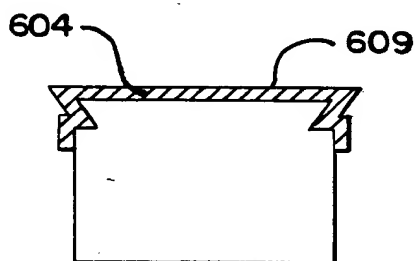


FIG. 2B

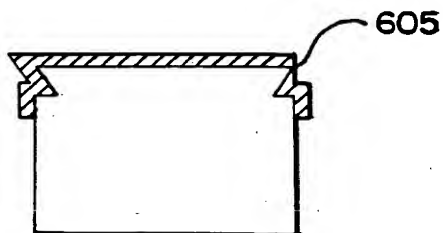


FIG. 2C

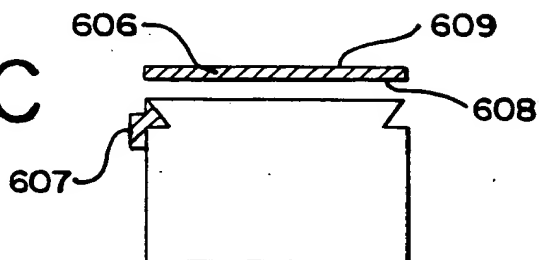
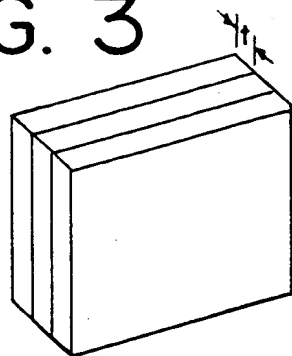


FIG. 3



PLATES STACKED FOR RULING

FIG. 3A

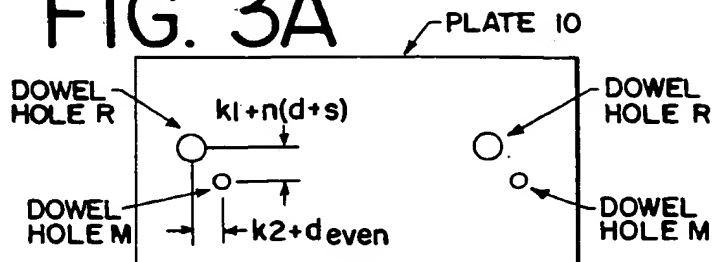


FIG. 4

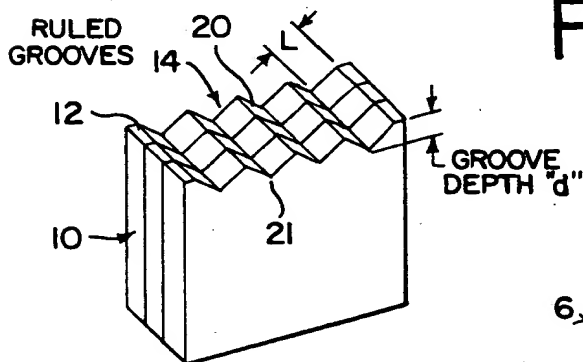


FIG. 5

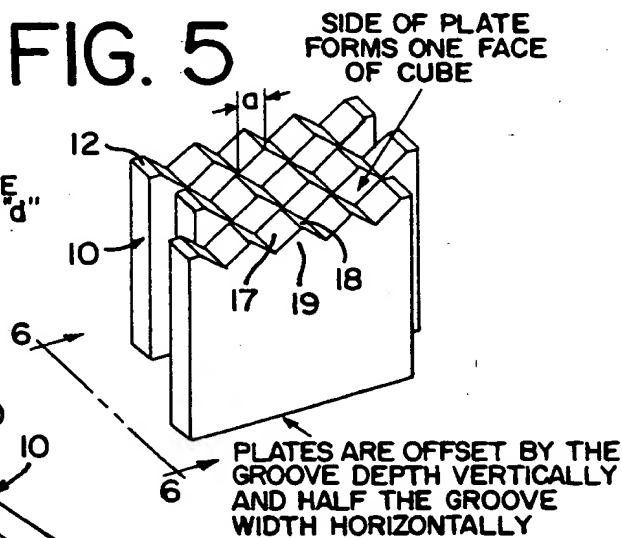


FIG. 6A

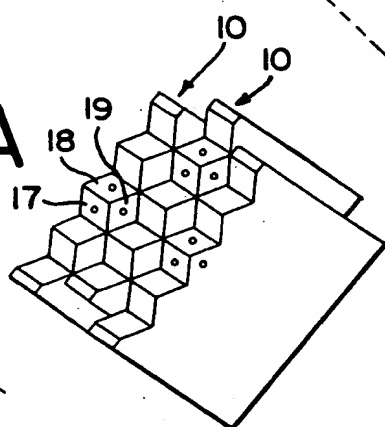


FIG. 6

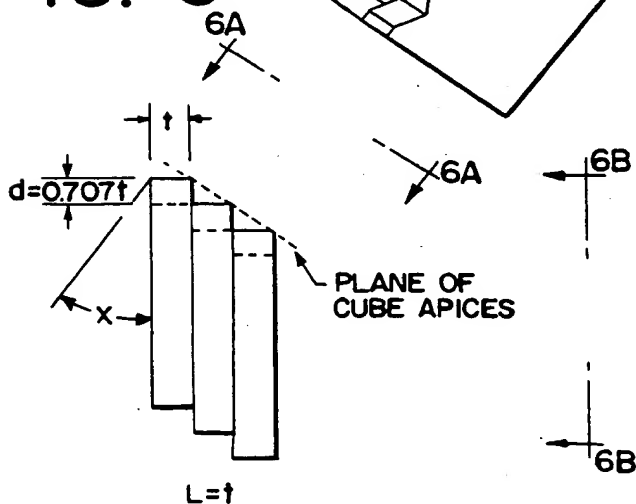


FIG. 6B

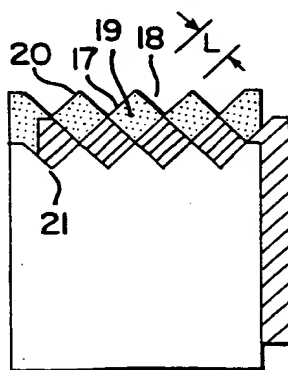


FIG. 7A

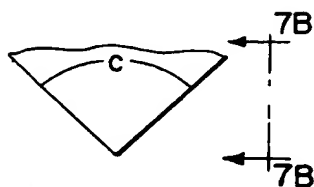


FIG. 7B



FIG. 9

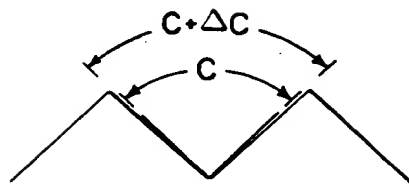


FIG. 8A

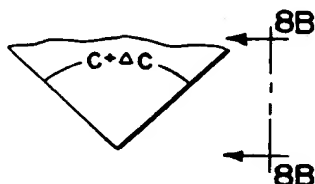


FIG. 8B

TOOL DIRECTION DURING CUTTING

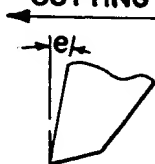


FIG. 10A

PROJECTION ALONG
CUBE DIAGONAL

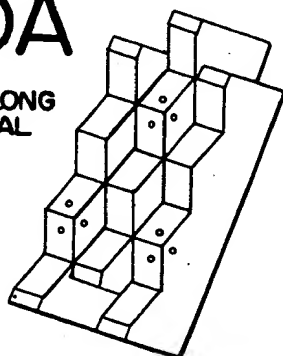


FIG. 10B

PROJECTION PERPENDICULAR
TO THE PLANE OF THE CUBE APICES

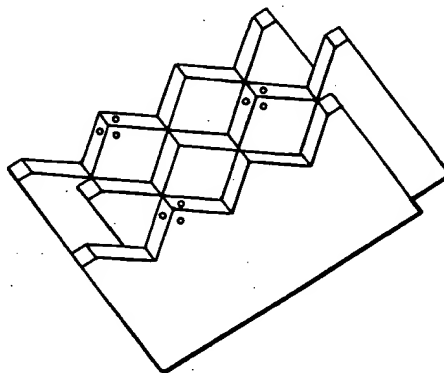


FIG. 10

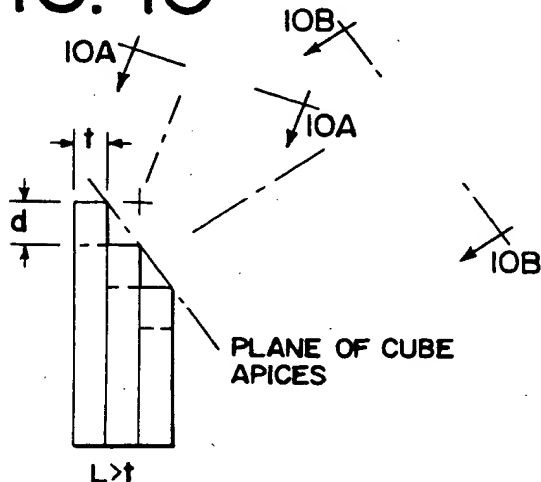


FIG. 10C

PROJECTION PERPENDICULAR
TO FACE OF PLATE

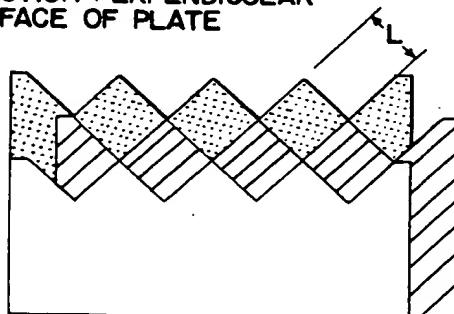


FIG. 11A

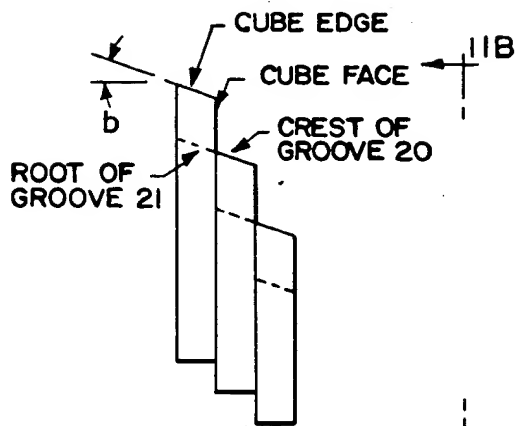


FIG. 11B

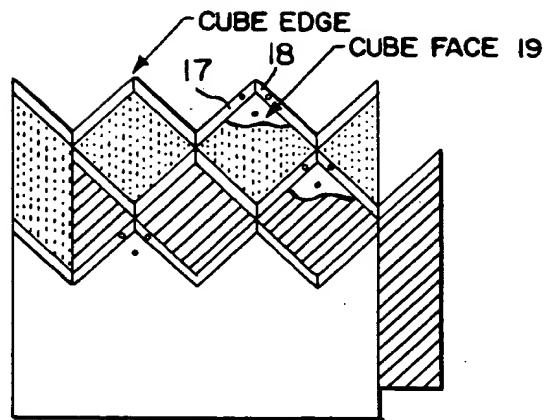


FIG. 11

PLATE ANGLE HIGHLY EXAGGERATED

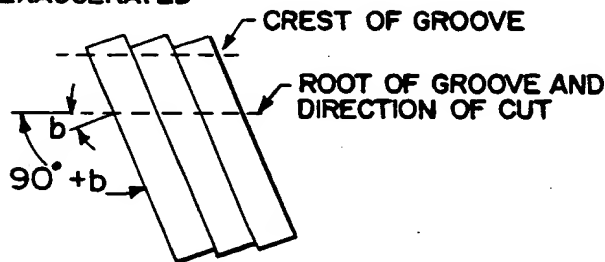


FIG. 12A

PROJECTION ALONG CUBE DIAGONAL

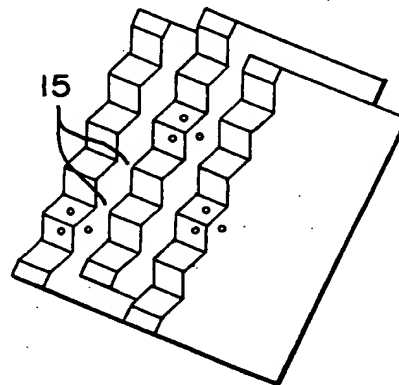


FIG. 12B

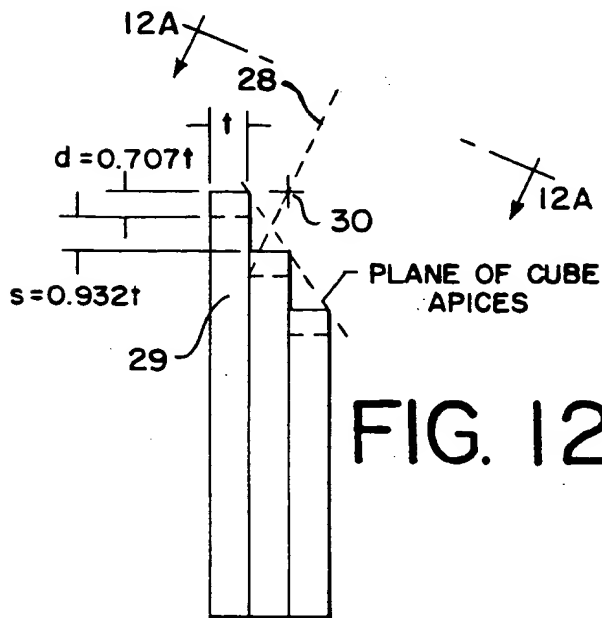
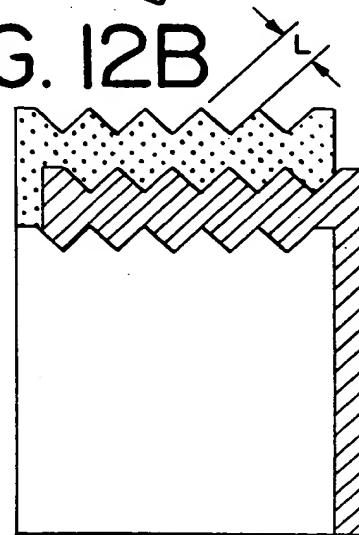


FIG. 12

PLATES DISPLACED SO GROOVE
EDGE DOES NOT MEET GROOVE
ROOT OF ADJACENT PLATE $L=t$

PROJECTION PERPENDICULAR
TO FACE PLATE

FIG. 12C

INTERRELATIONSHIP OF
d, s, t, I AND I'
FOR NEGATIVE VALUES OF I

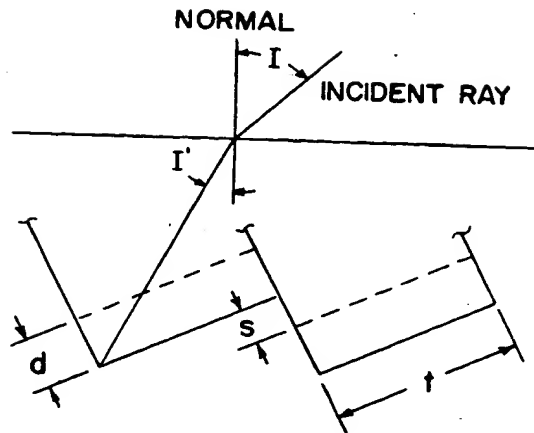


FIG. 12D

INTERRELATIONSHIP OF
d, s, t, I AND I'
FOR POSITIVE VALUES OF I

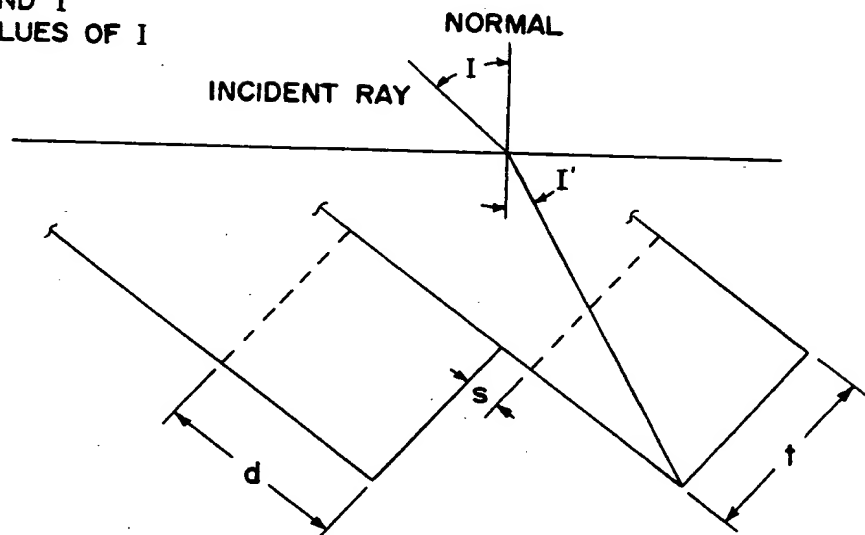
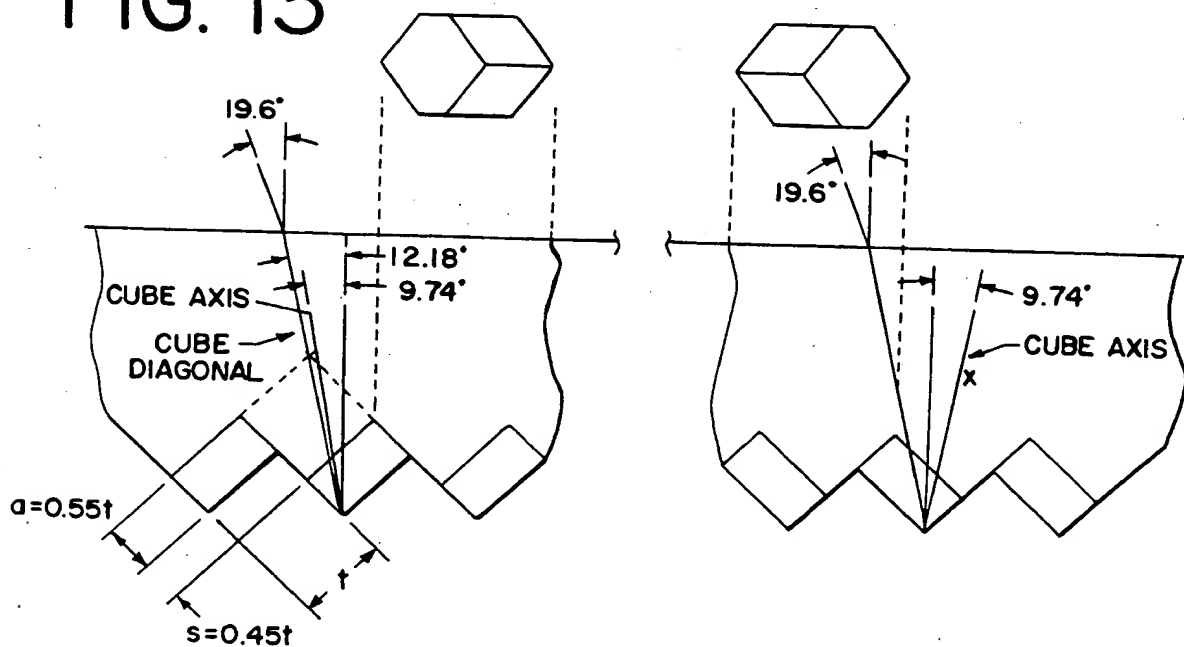


FIG. 13



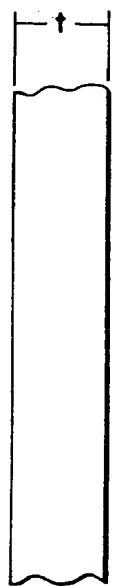
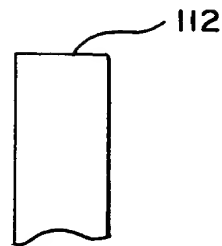


FIG. 14A

FIG. 14B



110

FIG. 15

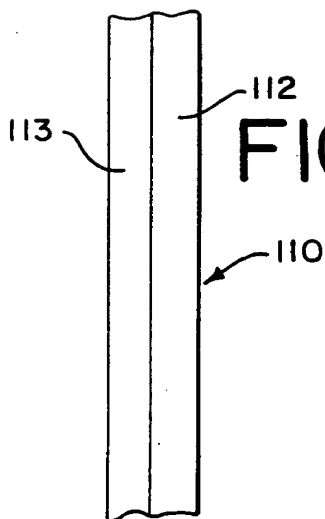
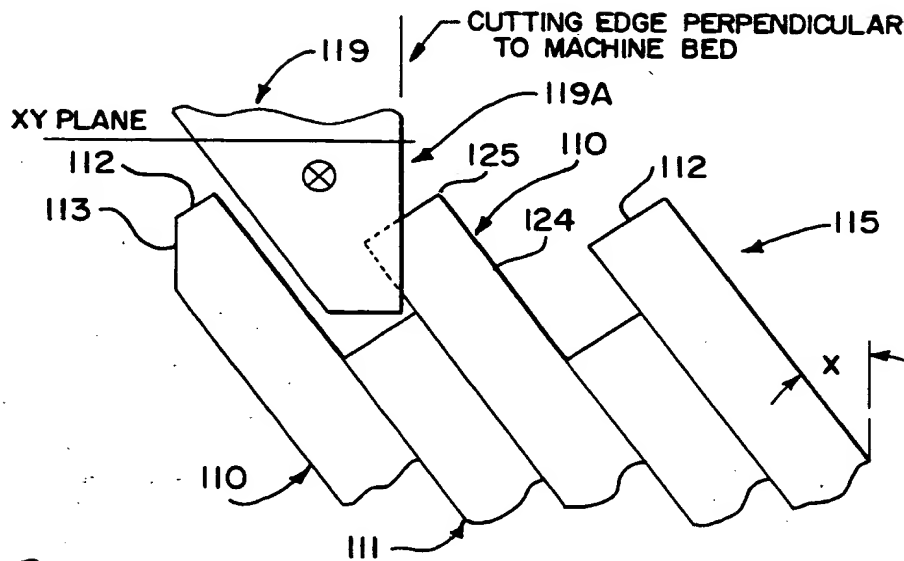


FIG. 16A

FIG. 16B

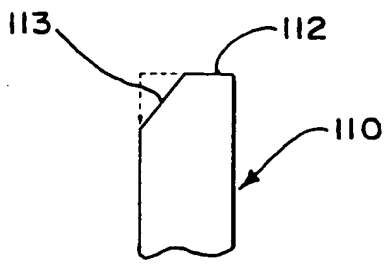


FIG. 17

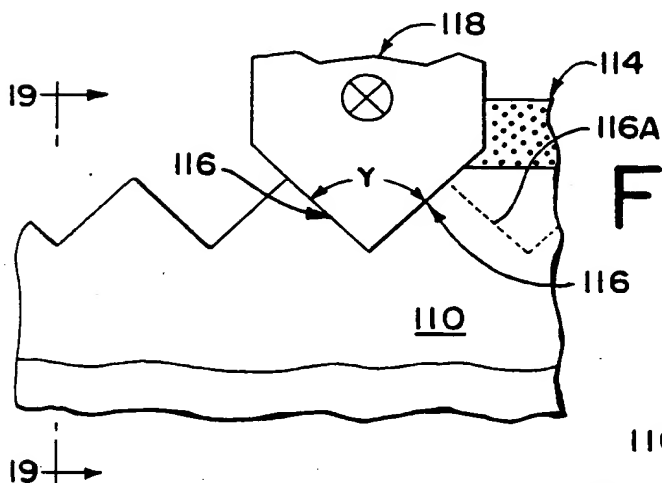
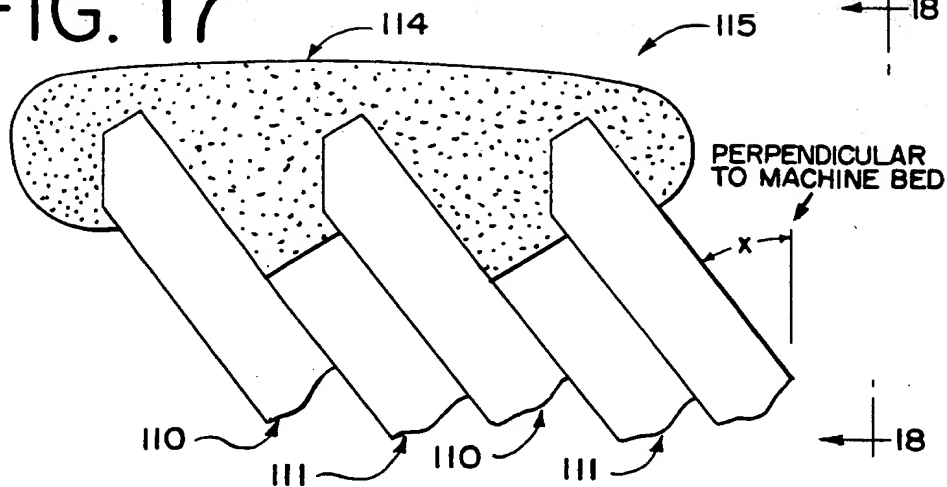


FIG. 18

FIG. 21

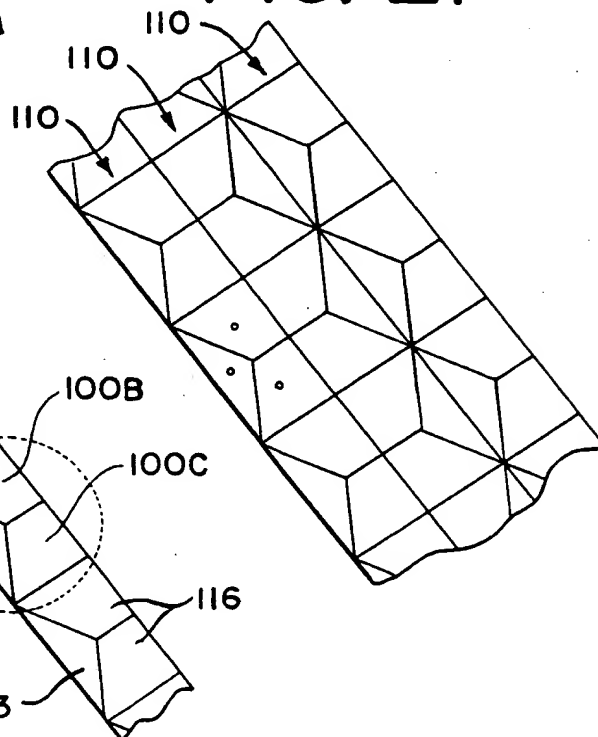


FIG. 20

FIG. 19

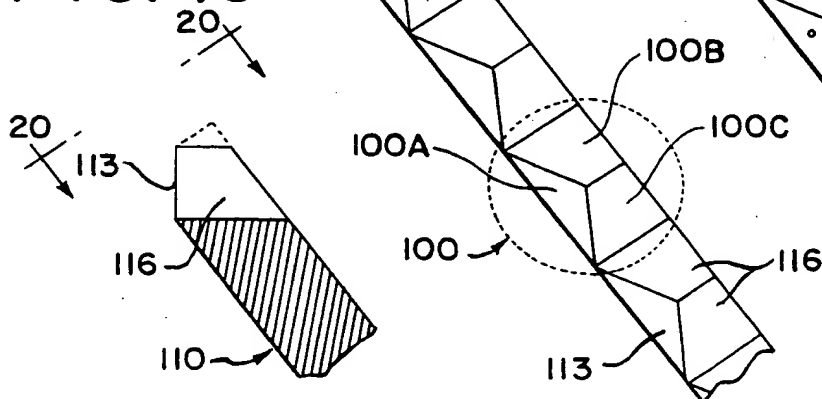


FIG. 22A

TOOL CUTTING EDGE
PERPENDICULAR TO
MACHINE BED

FIG. 22B

FIG. 22C

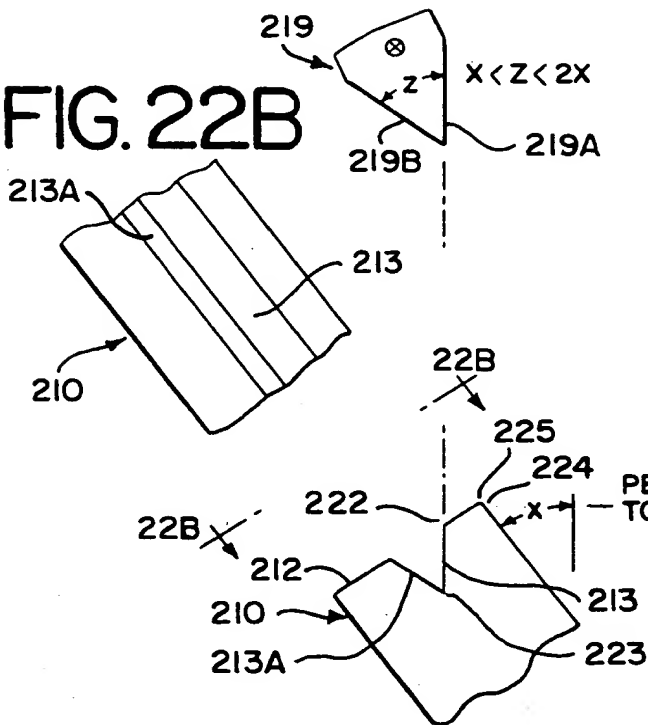
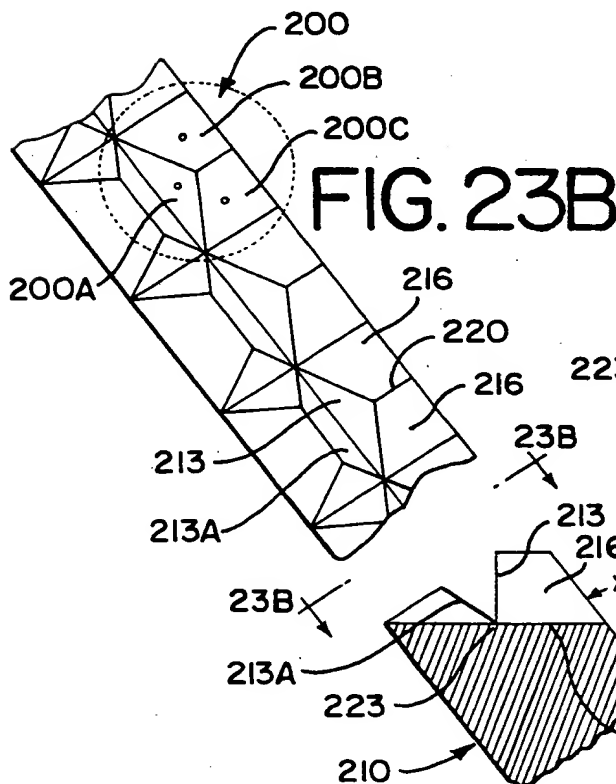


FIG. 22

FIG. 23



TOOL FOR
FACES 216

FIG. 23A

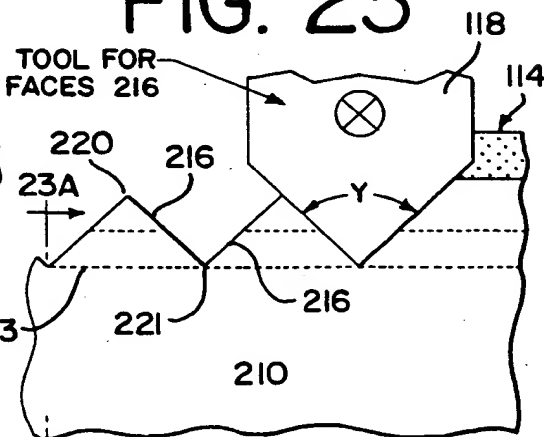


FIG. 25B

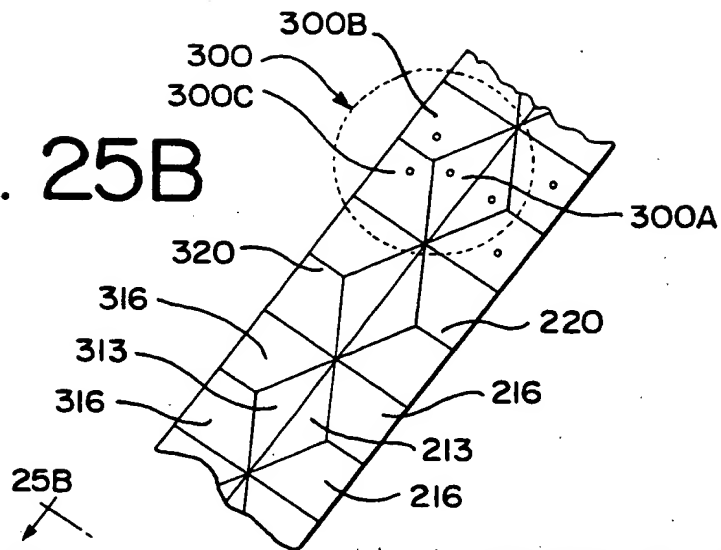


FIG. 25A

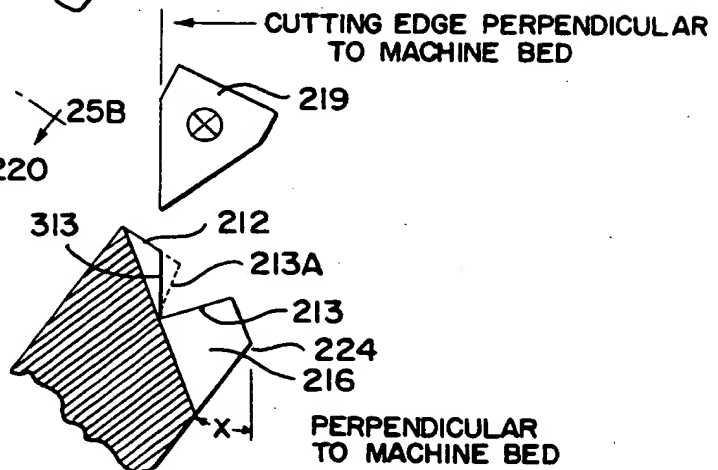
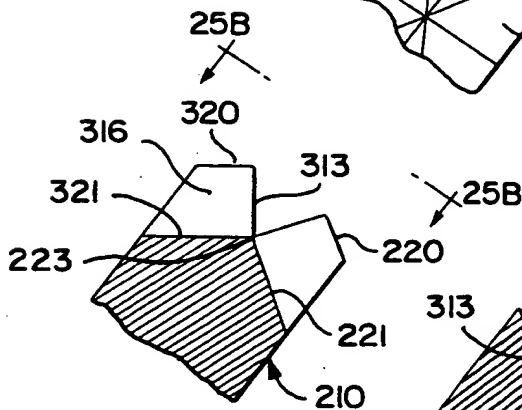


FIG. 24

FIG. 25

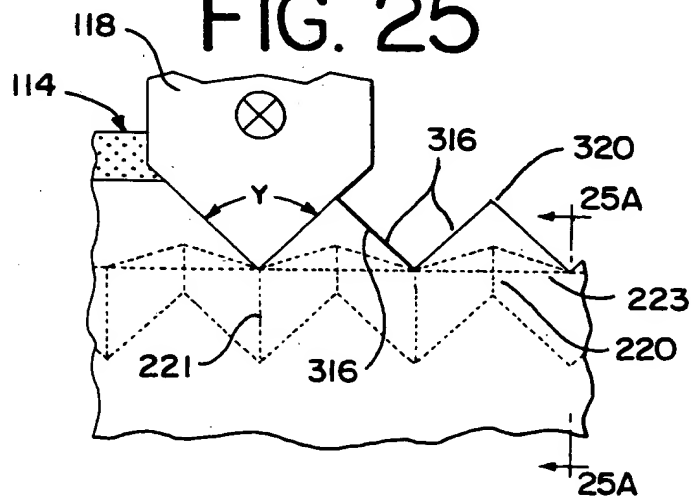


FIG. 26

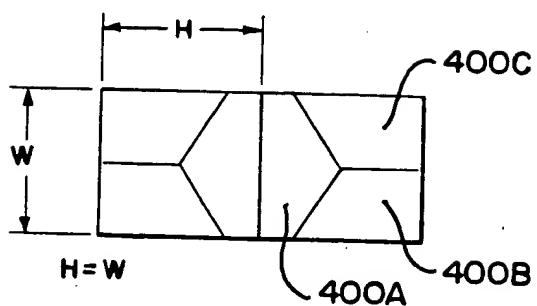


FIG. 27B

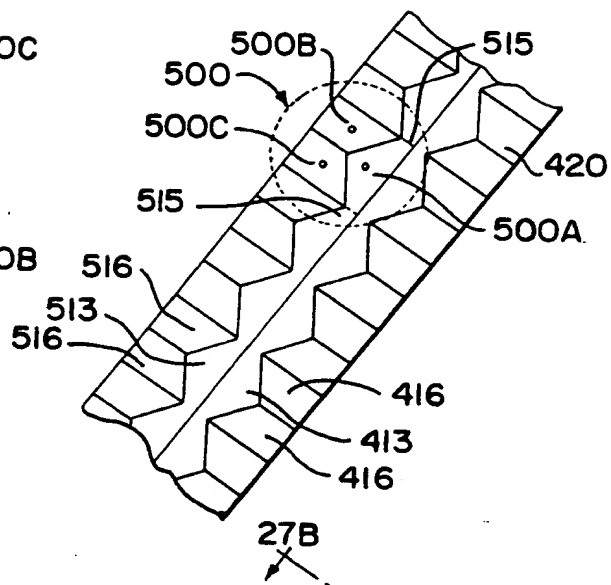


FIG. 27

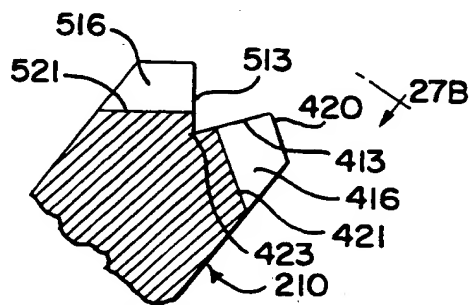
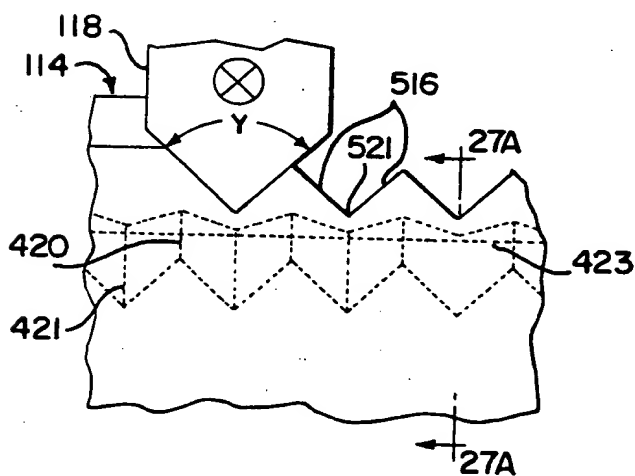


FIG. 27A

FIG. 27C

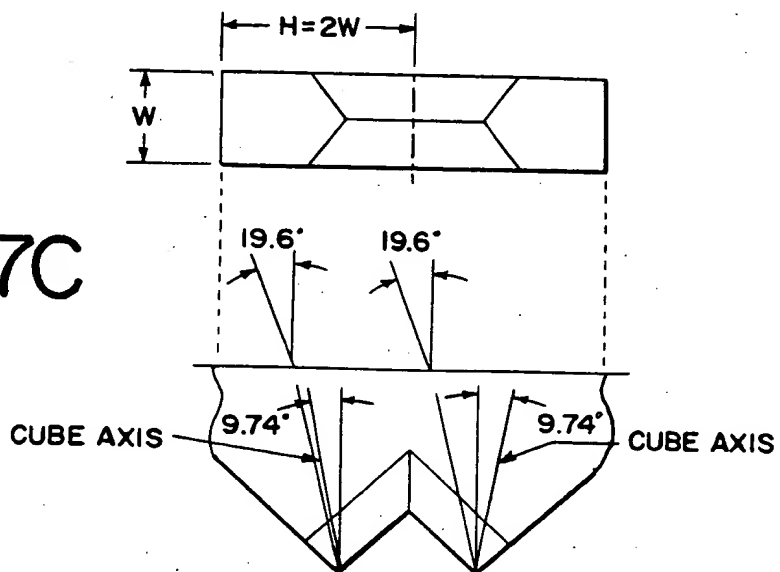
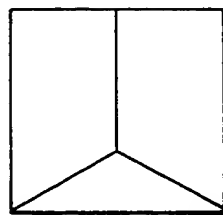
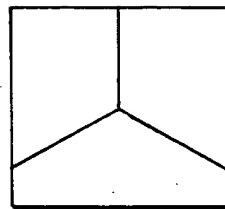


FIG. 28

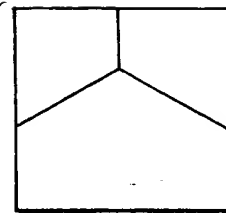
APEX
DECENTRATION



TOWARDS FACE,
58% ACTIVE

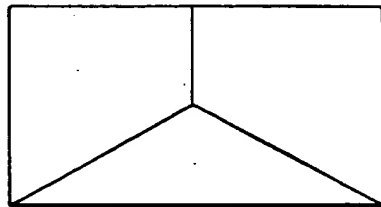


CENTERED,
100% ACTIVE

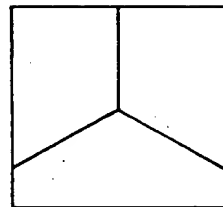


TOWARD EDGE,
58% ACTIVE

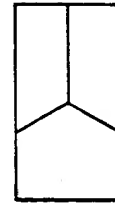
BOUNDARY
PROPORTIONS



1.73:1

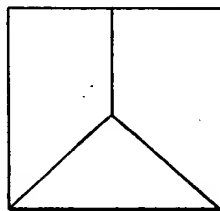


SQUARE

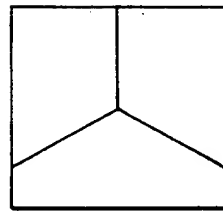


1:2

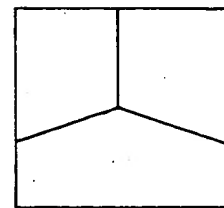
AXIS
CANT



CANT = -9.74°



UNCANTED



CANT = +15°

FIG. 29A

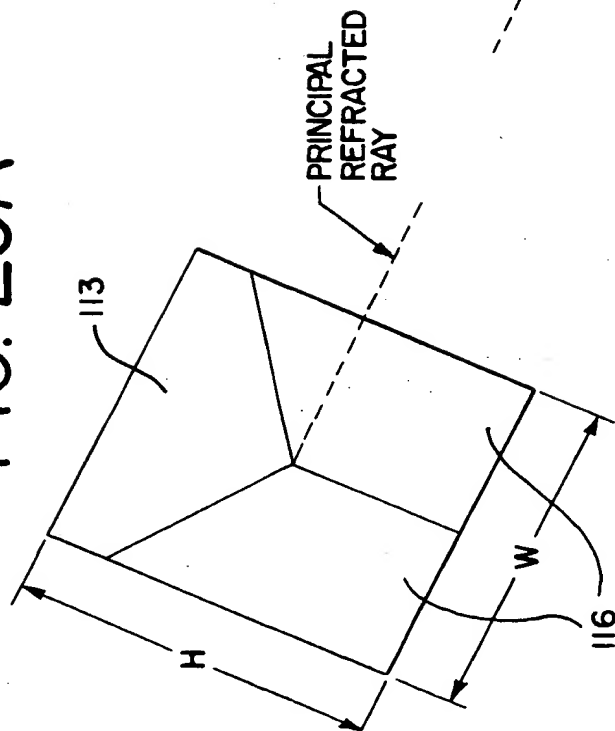


FIG. 29

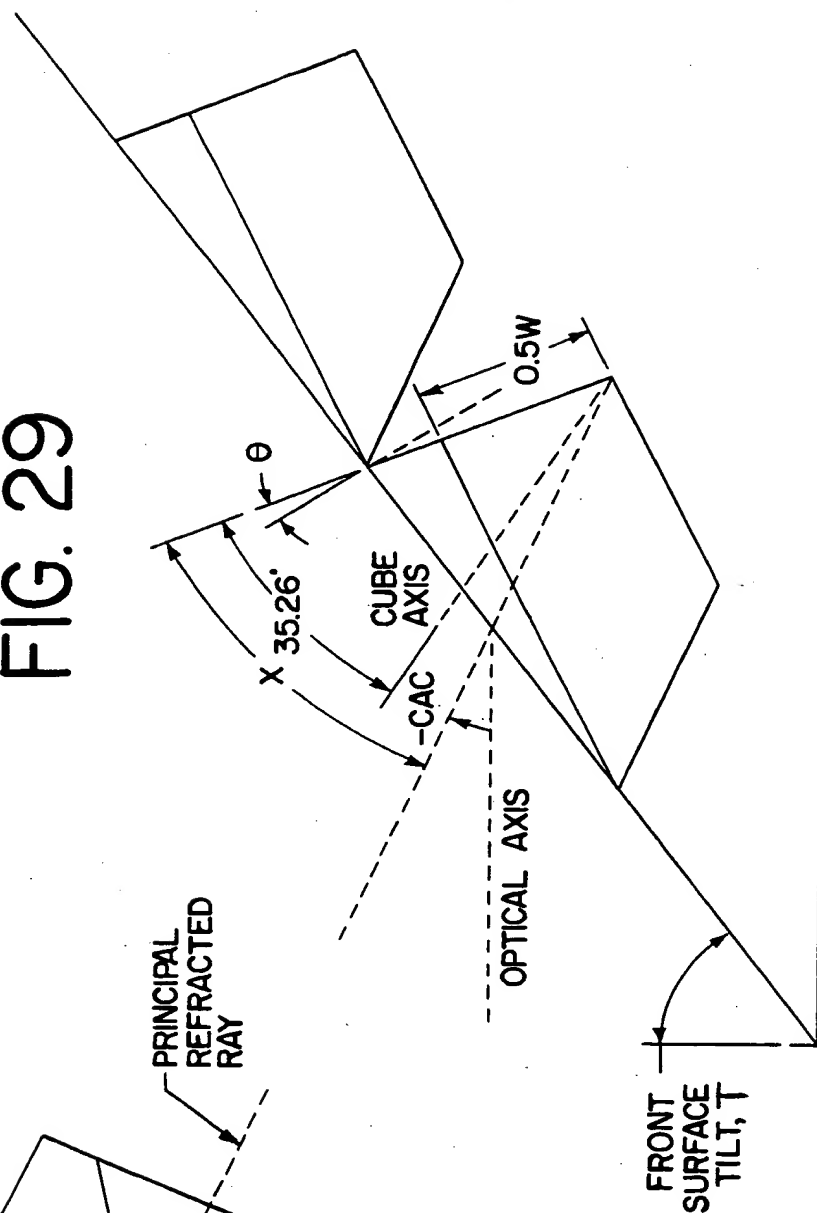


FIG. 30

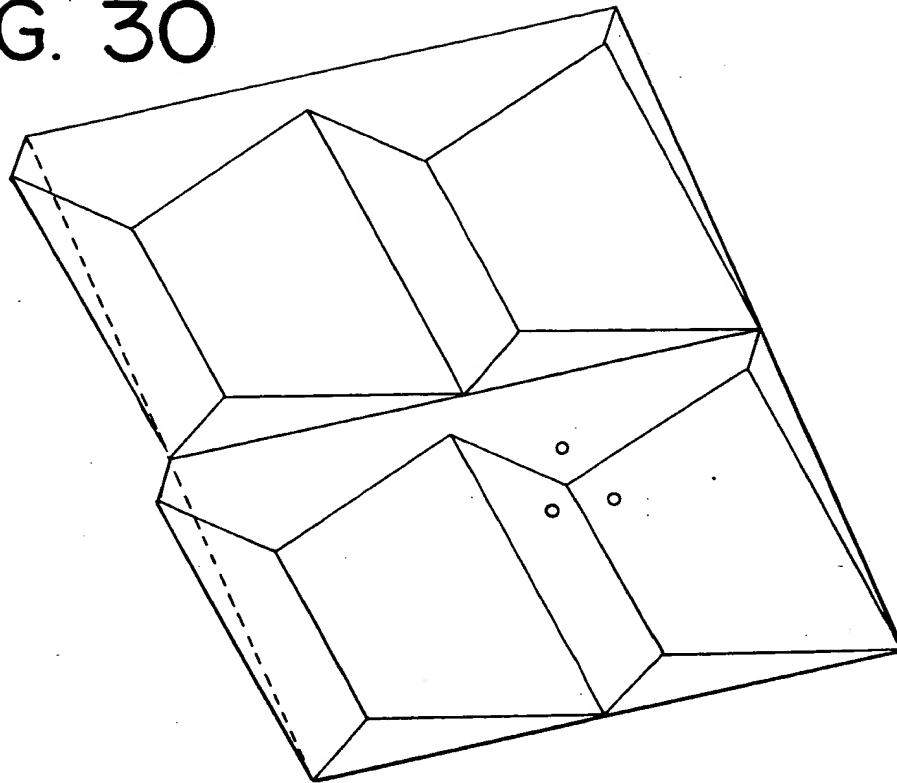


FIG. 31

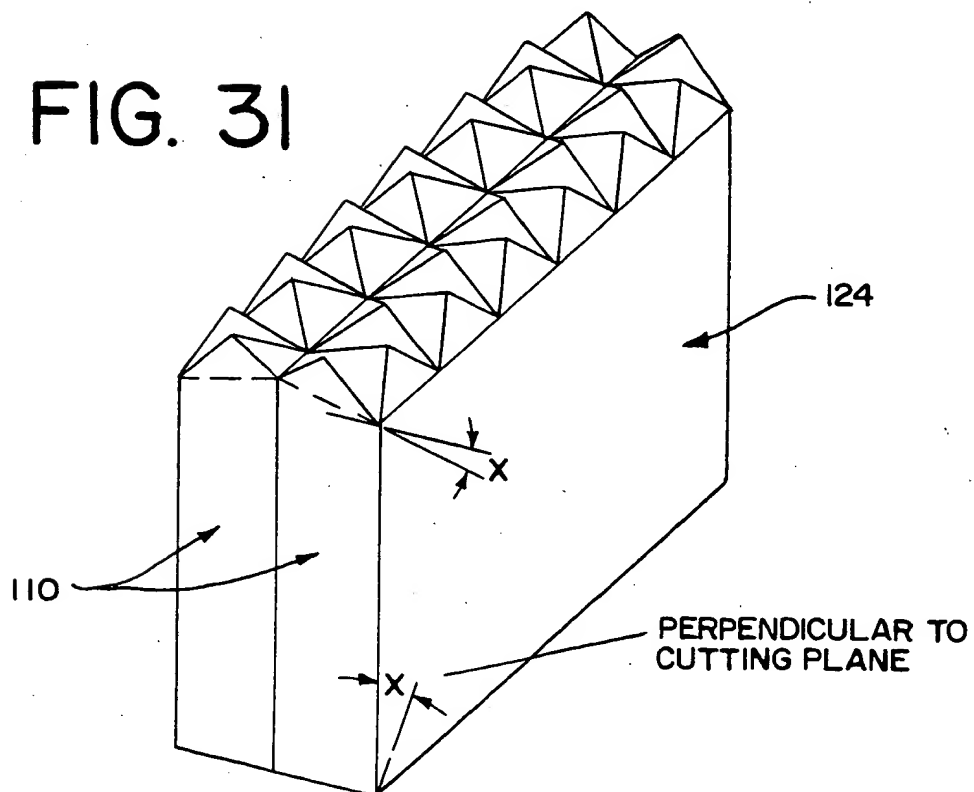


FIG. 32

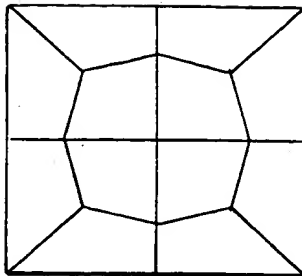


FIG. 33

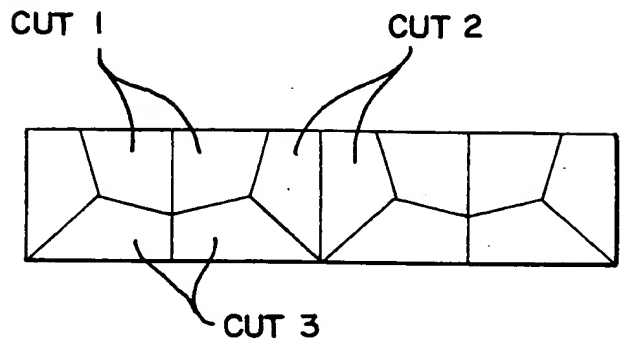


FIG. 34A

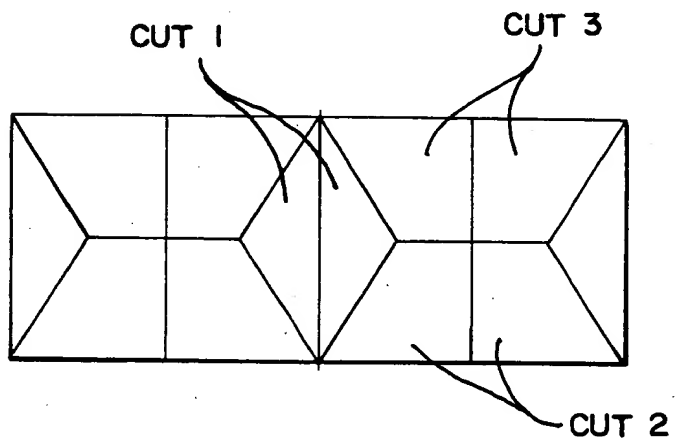


FIG. 34B

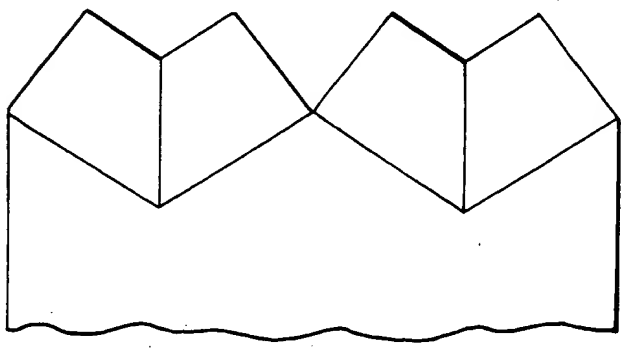


FIG. 35 ARRAY OF PENTA-FACE HEXAGONAL CUBES SHOWING A PLATE HIGHLIGHTED

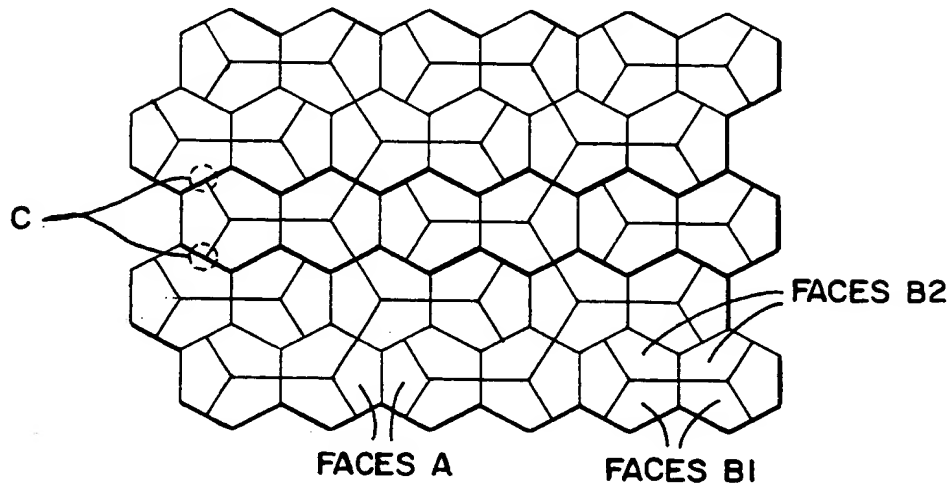


FIG. 36

ARRAY OF PENTAGONAL CUBES WITH
+8.7 AXIS TILT AND 89.8 AREA EFFICIENCY

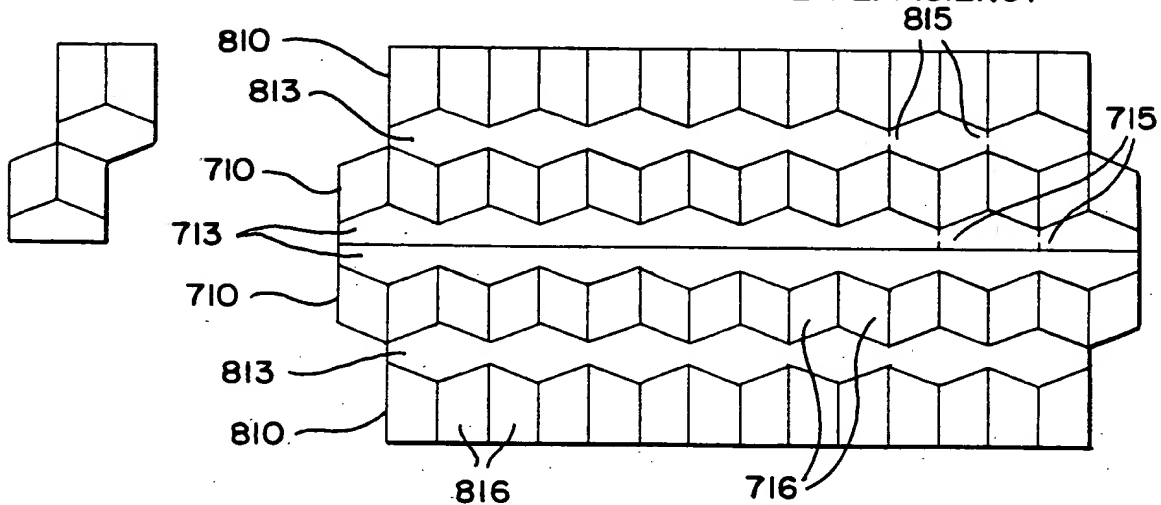
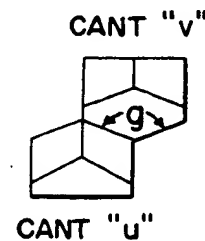


FIG. 36A



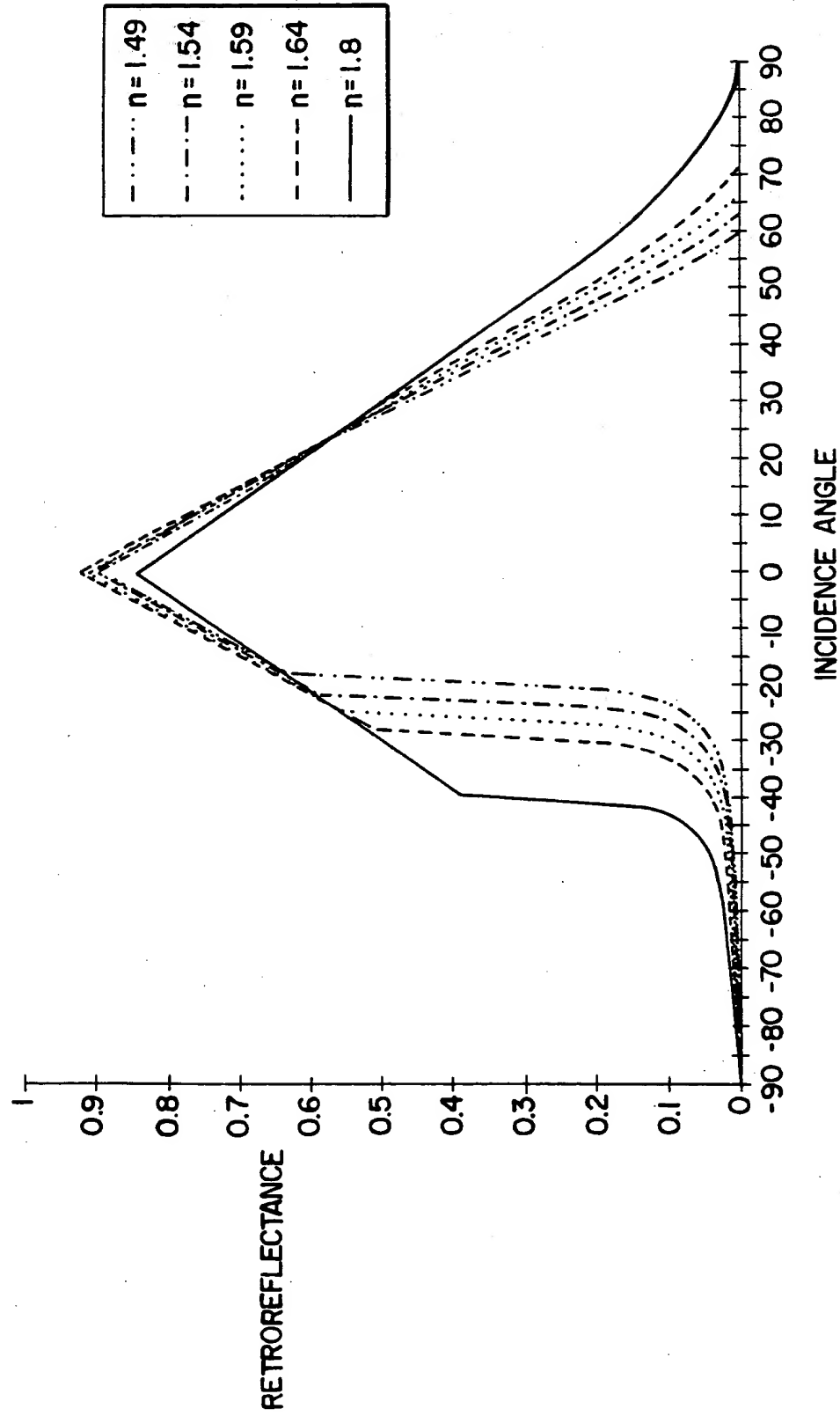
$$g = 2 \arctan \frac{\sqrt{3} \cos(v-u)}{\cos(v) - \sqrt{2} \sin(v)}$$

SECRET 6663100

APPROVED	BY	RECLASS
	DRAFTSMAN	

FIG. 37

PERFORMANCE OF SIMPLEST HEXBLADE ARRAY ($d/\lambda = .7071$, $s/\lambda = 0$, NOT PAIRED)
FORMED IN MATERIALS OF DIFFERENT REFRACTIVE INDICES



66667 666666

PROJECT
BY
DRAFTSMAN
CLASS

FIG. 38

PERFORMANCE OF HEXBLADE ARRAYS ($n=1.49$, $s/t=0$, NOT PAIRED)
OPTIMIZED FOR DIFFERENT INCIDENCE ANGLES

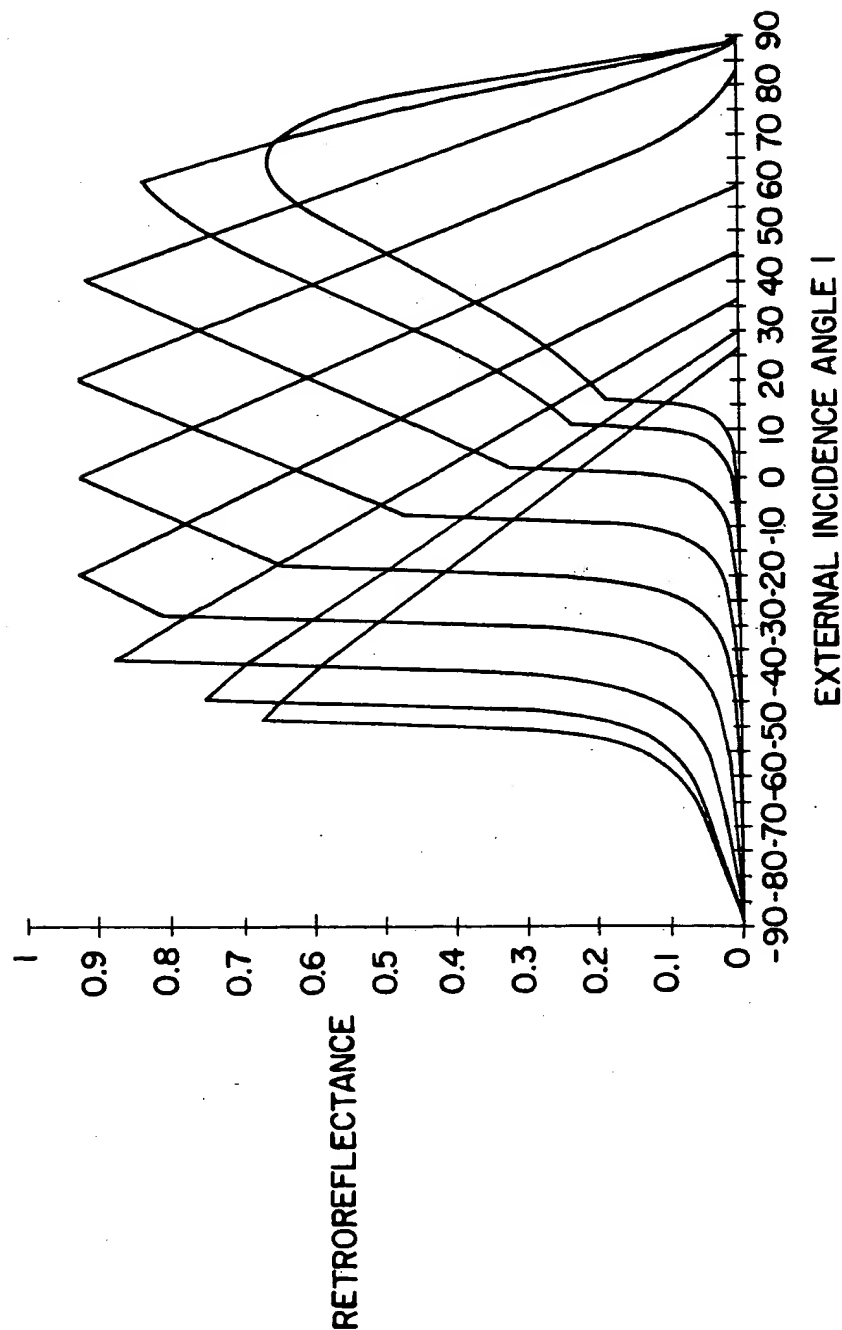


FIG. 39

PERFORMANCE OF HEXBLADE ARRAYS ($n=1.49$, $s/t=0$, NOT PAIRED)
OPTIMIZED FOR DIFFERENT INCIDENCE ANGLES

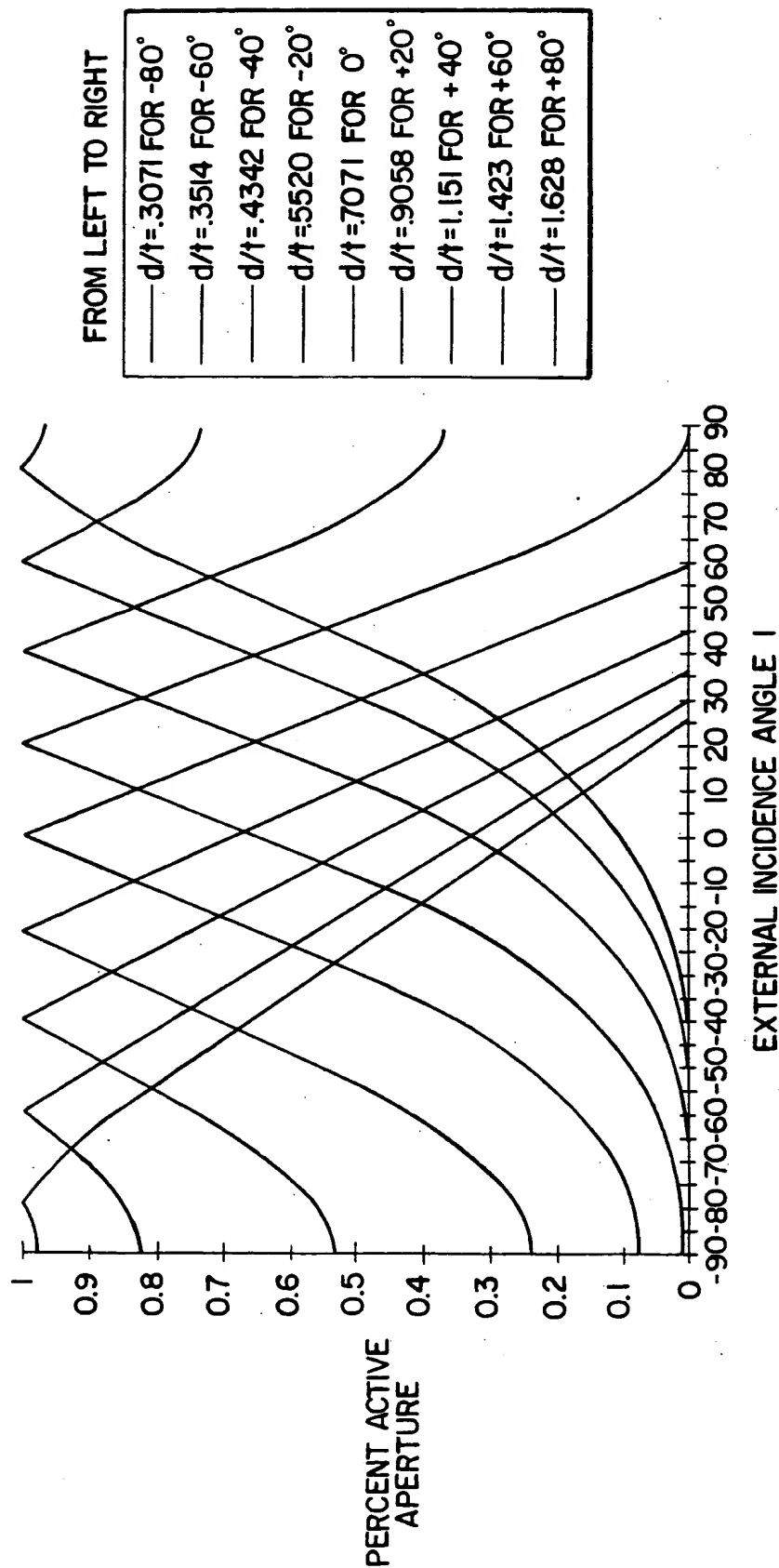


FIG. 40

RECTANGLE AND HEXAGON MICROCUBES OF EXAMPLE 1 (REFRACTIVE INDEX = 1.59)

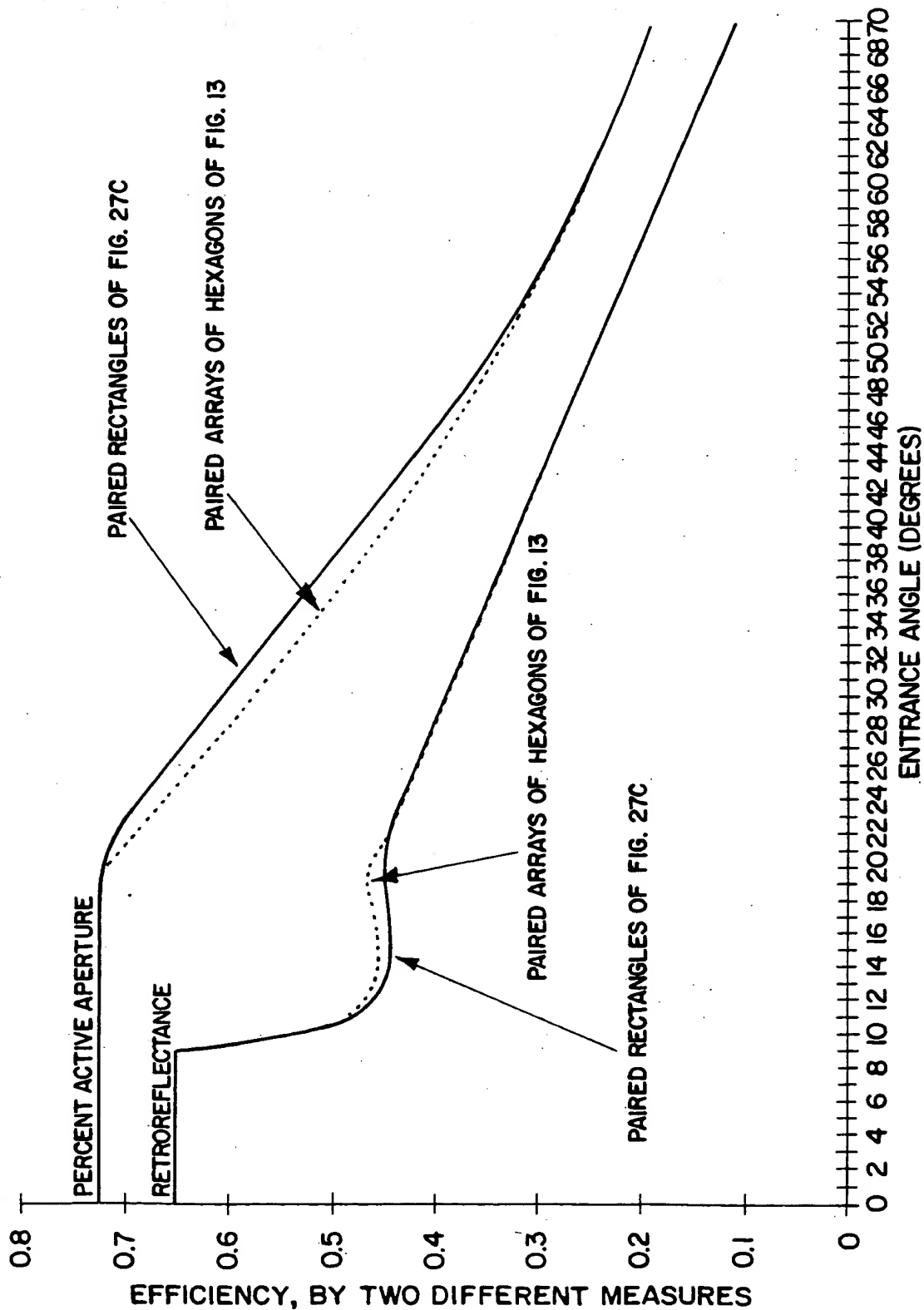


FIG. 41

PERFORMANCE OF RECTANGLE CUBES ($n=1.49$) IN A RAISED
PAVEMENT MARKER (FRONT FACE 55 DEG. TO VERTICAL)

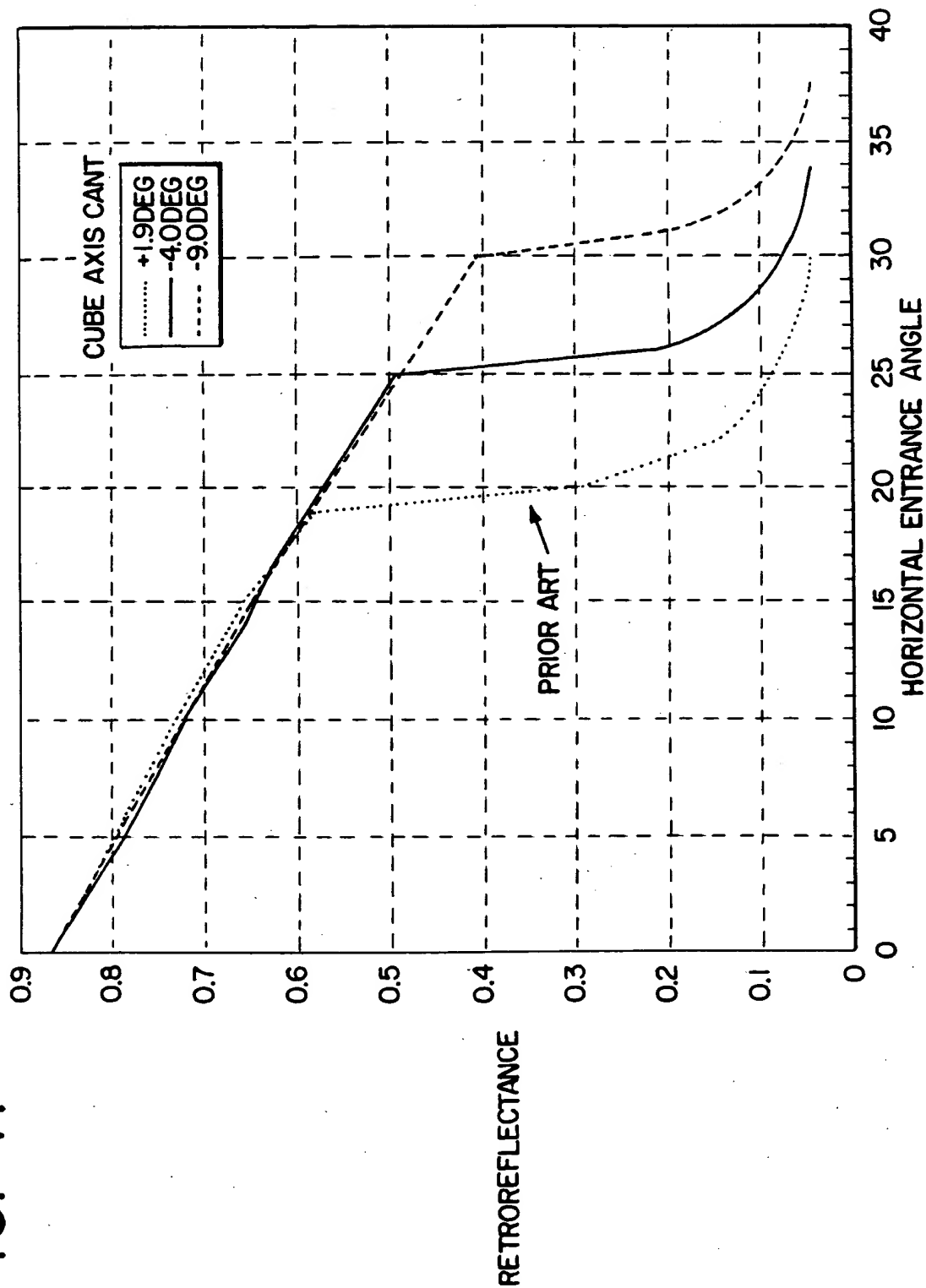


FIG. 42A

RETROREFLECTANCE VERSUS ENTRANCE
ANGLE FOR PAIRED ARRAYS 0

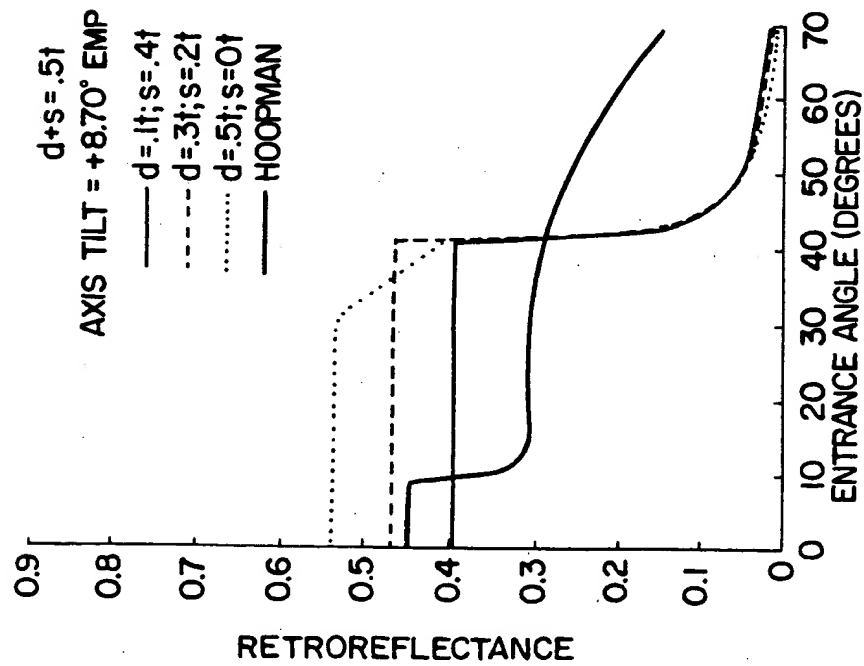


FIG. 42B

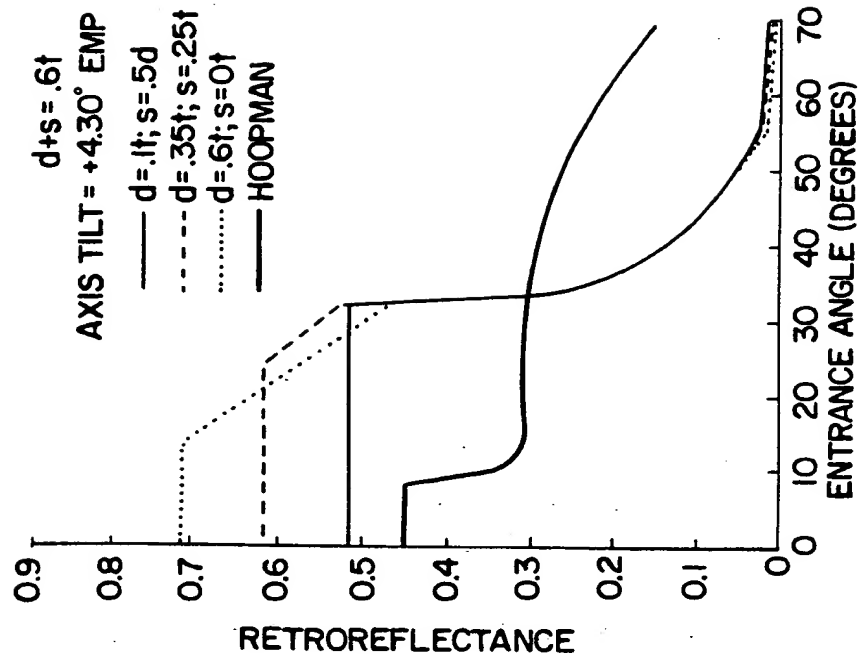


FIG. 42C

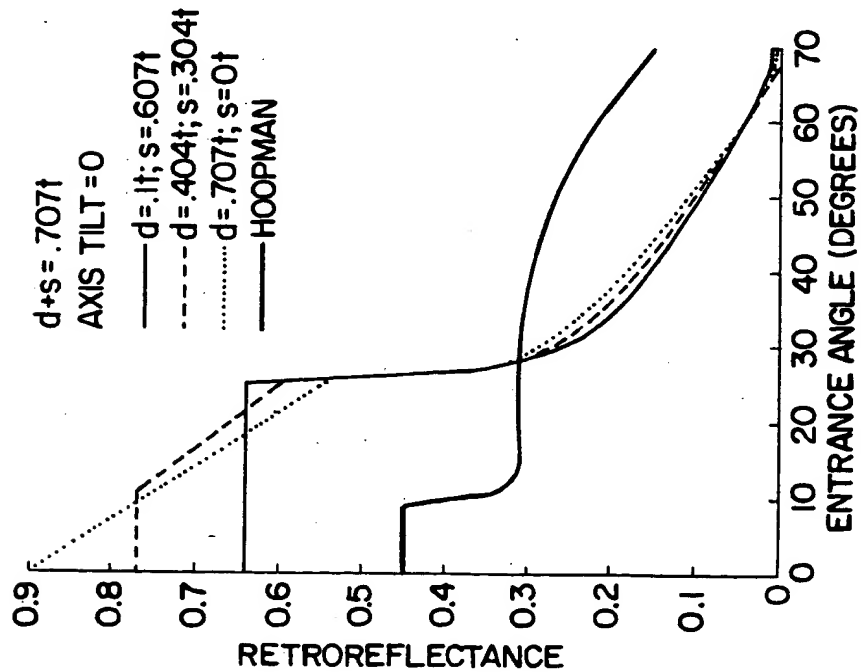


FIG. 42D

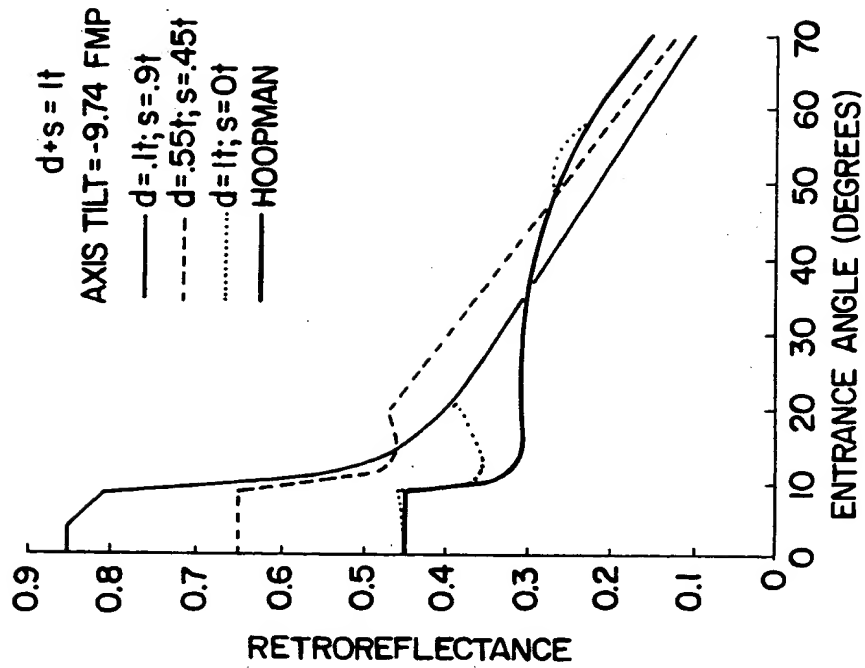


FIG. 42E

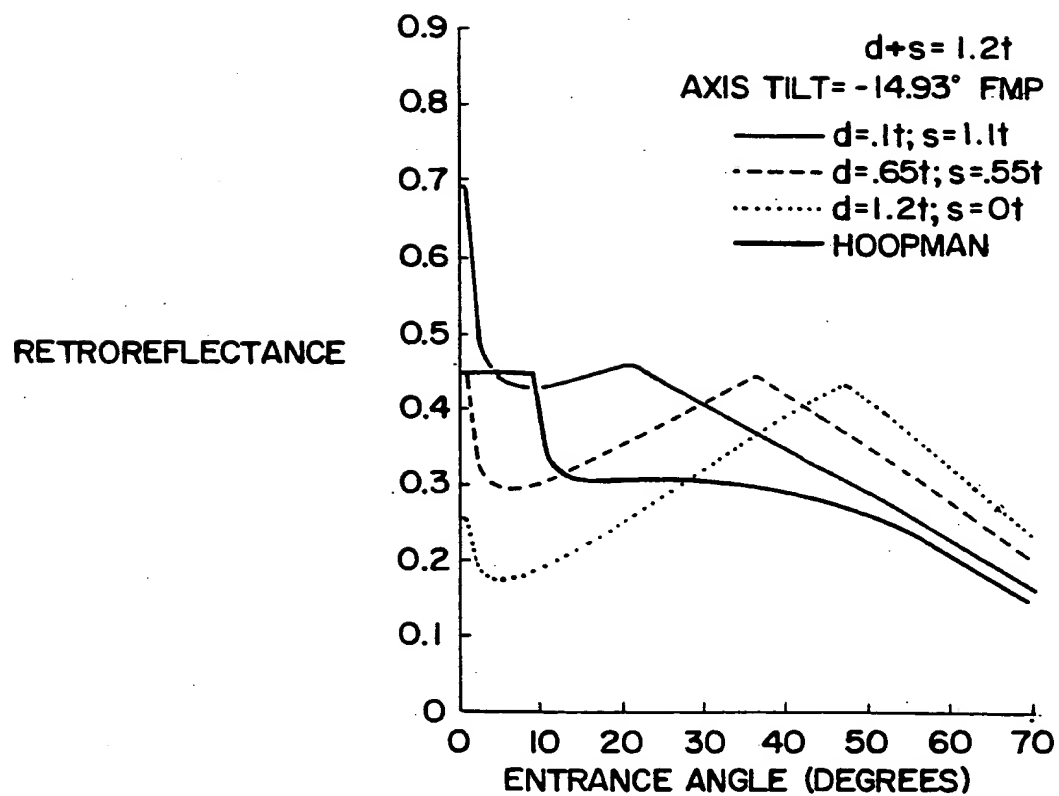


FIG. 43

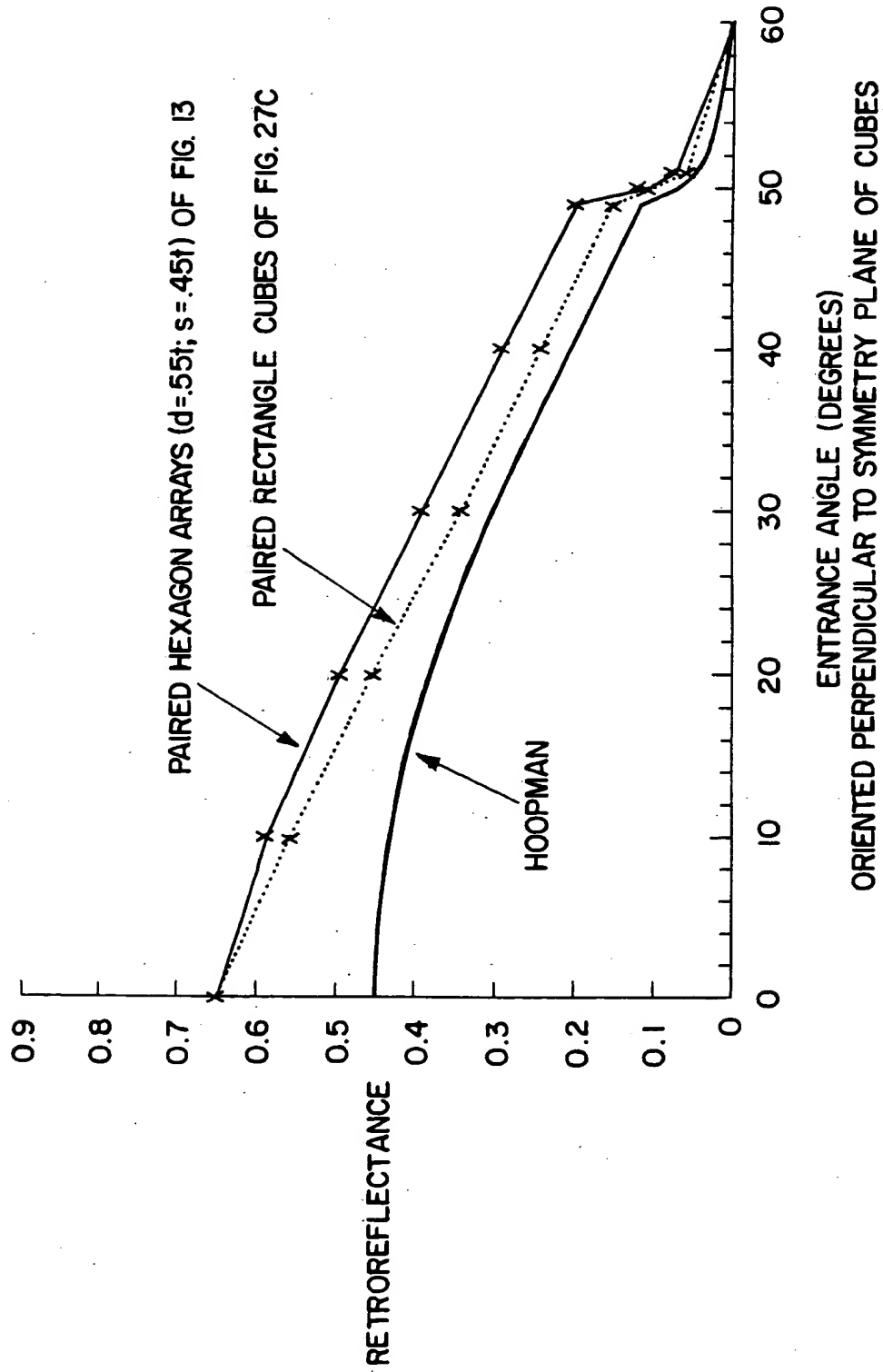


FIG. 44

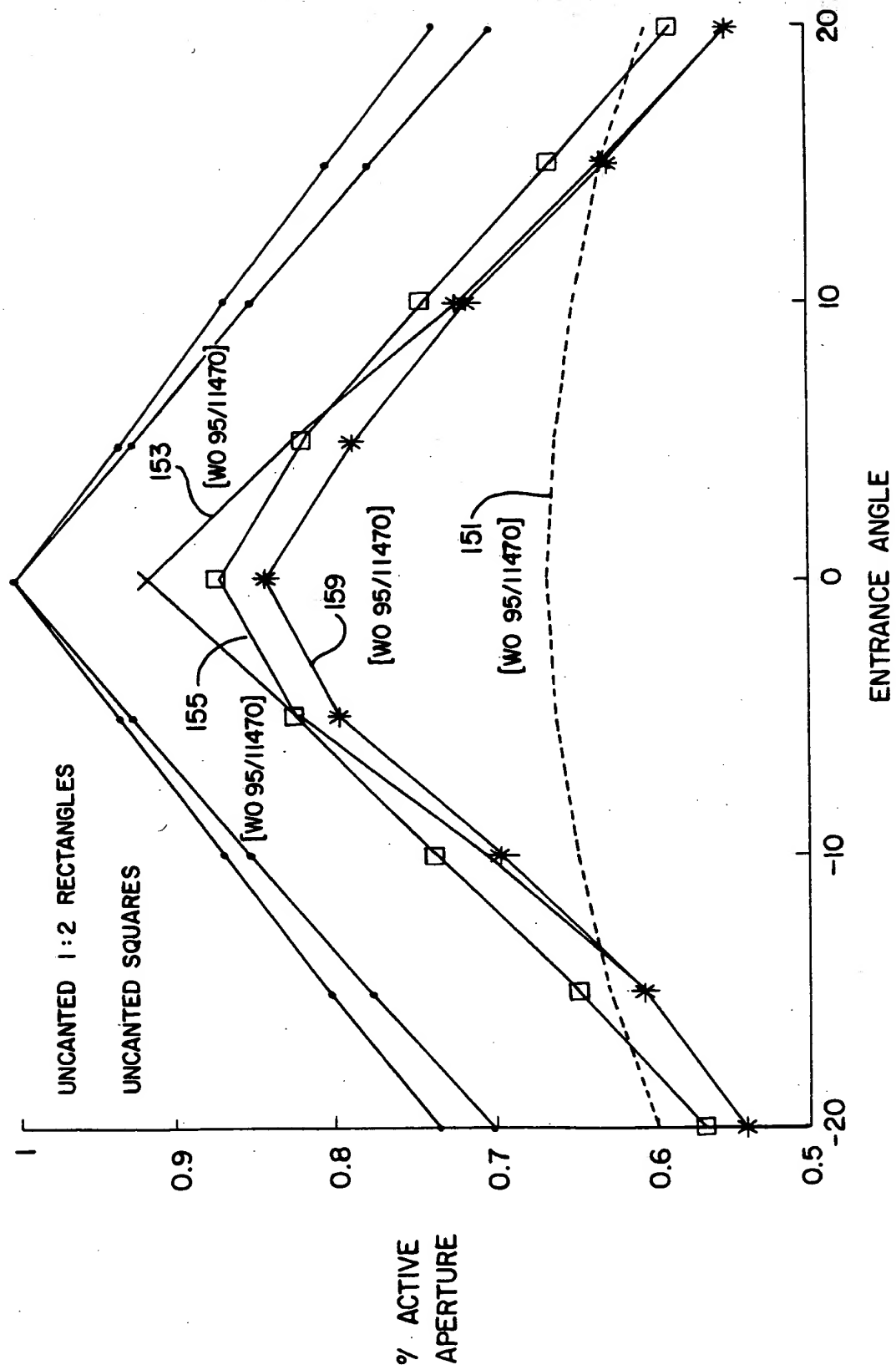


FIG. 45

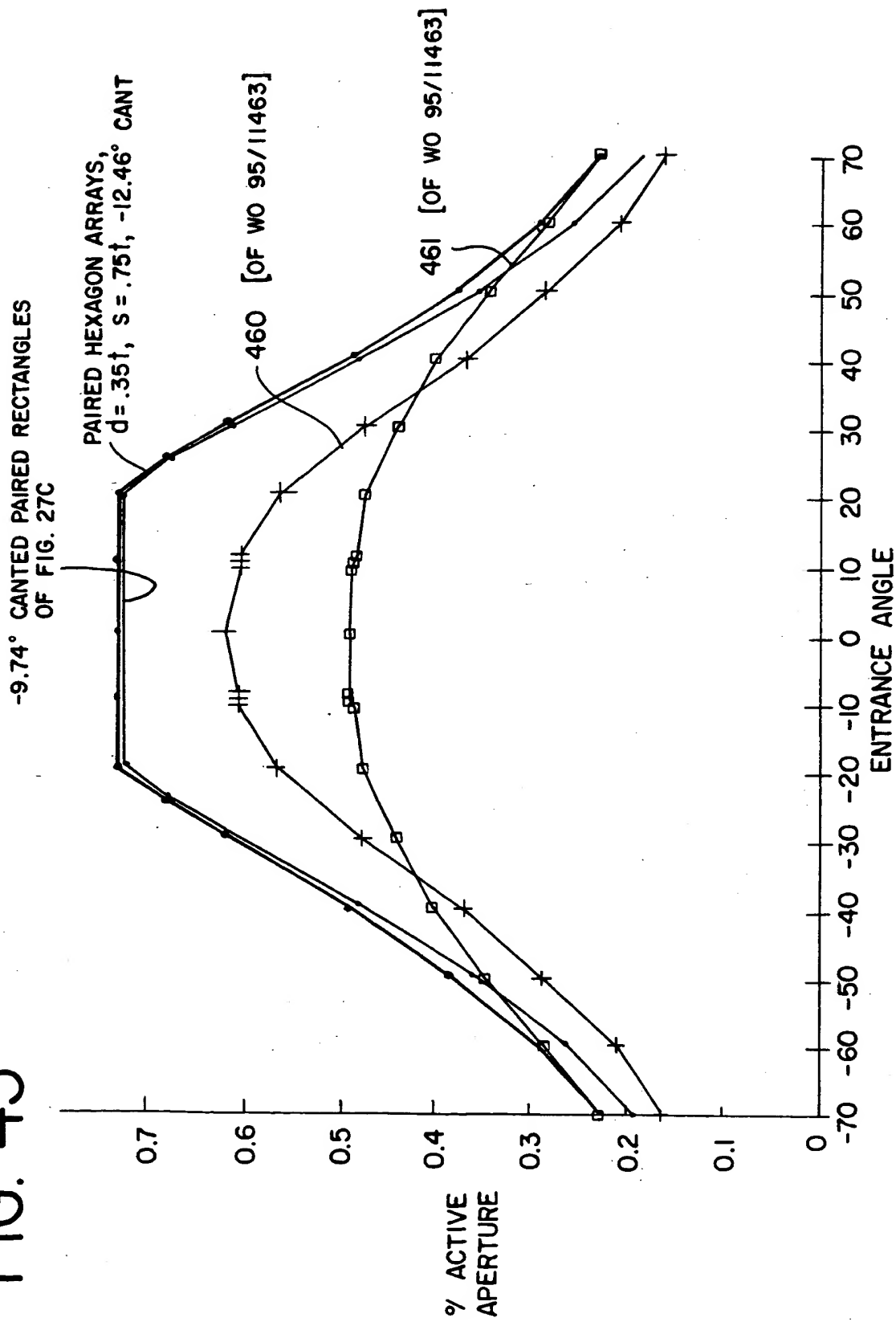


FIG. 46a

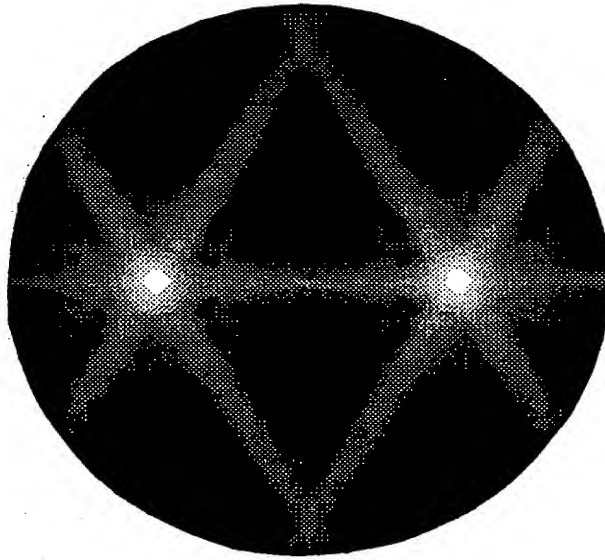


FIG. 46b

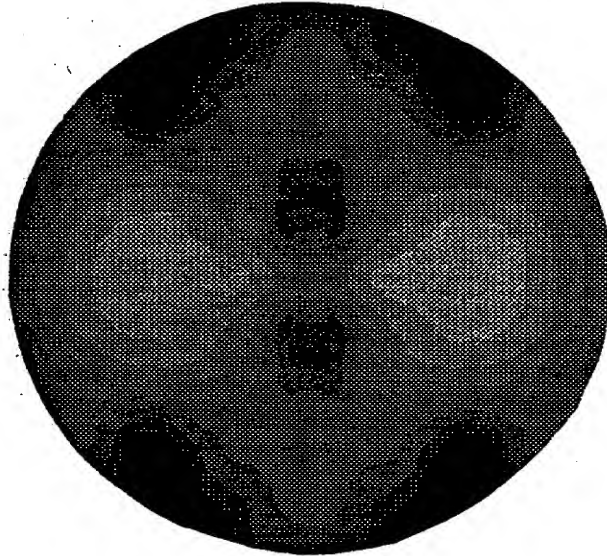


FIG. 46c

